Fuel Tank Flammability

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Background/Agenda

- In addition to LOC testing and in-flight flammability measurements, the FAA has several fuel tank flammability tests ongoing
- > We will discuss
 - Effects of fresh fuel leakage into a nearly empty, heated tank
 - Theoretical flammability limits as a function of MIE, flashpoint and O₂ Content
 - Combustion sphere testing

Flammability Effects of Fresh Fuel Leakage Into a Nearly Empty, Heated Tank

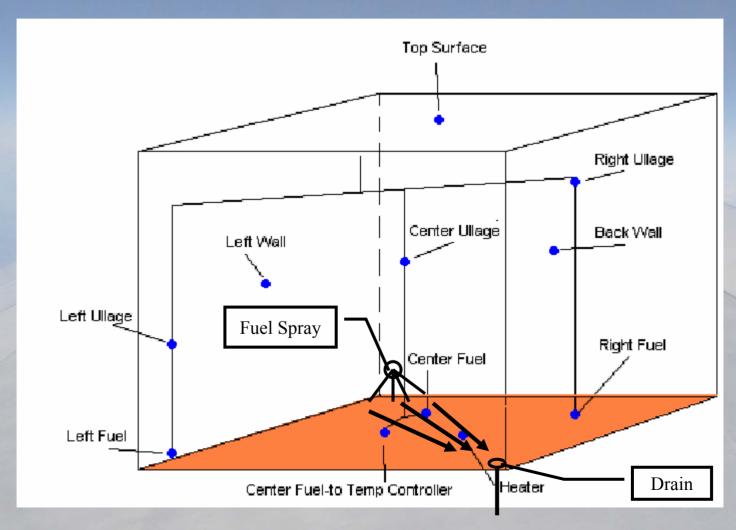
Objectives

- Previous tests have shown that in order to see a significant decrease in flammability, the mass loading of the tank must be driven down to 0.25 kg/m³ or less.
- If it were feasible to do this though, would fuel leaking in from other tanks be counterproductive to the flammability reduction.

Apparatus

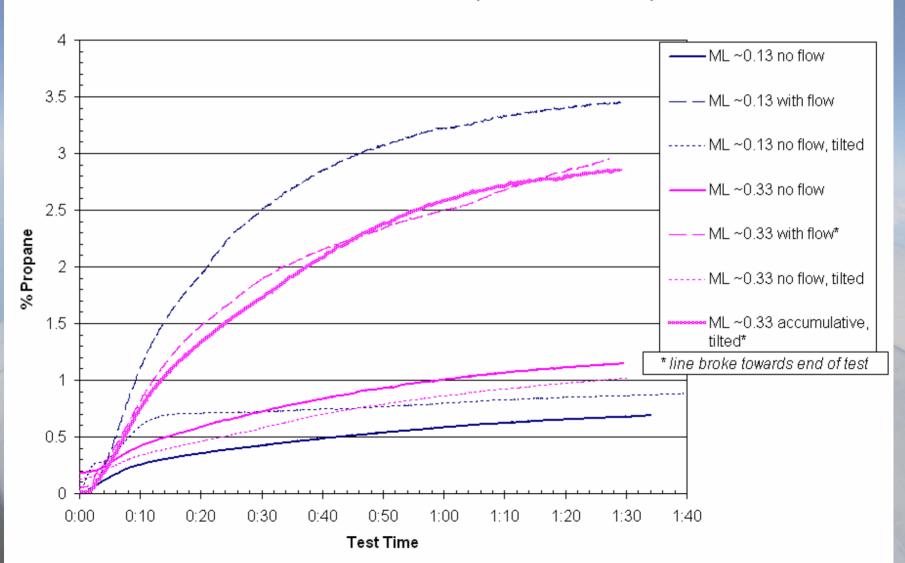
- ➤ Utilizing same tank as was used in the fuel condensation modeling work.
- Peristaltic pump used to pump fresh fuel into tank such that it sprays in at far side and traverses the entire bottom of the tank.
- Fuel inside of tank is continuously drained at approximately the same rate that fresh fuel is entering (~0.3 LPM).
- ➤ Bottom heater temperature is maintained at 180°F for approximately 1.5 hours.

Apparatus



Results





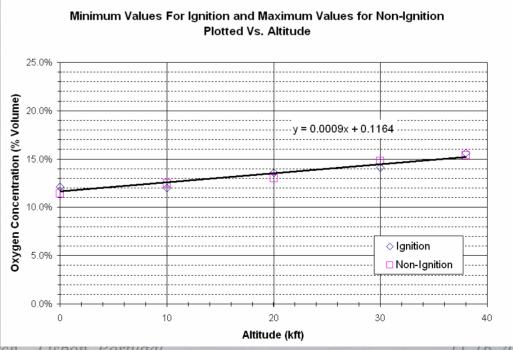
Conclusion

Flow of fresh fuel across the heated bottom surface of a tank negate the effects of a low fuel load by increasing THC (flammability) by a factor of 2.5 - 4.

Theoretical Flammability Limits as a Function of MIE, FP & O2 Content

Present thinking in fuel tank inerting is that above $x\% O_2$, the tank is at risk throughout the entire flammability envelope, below x%

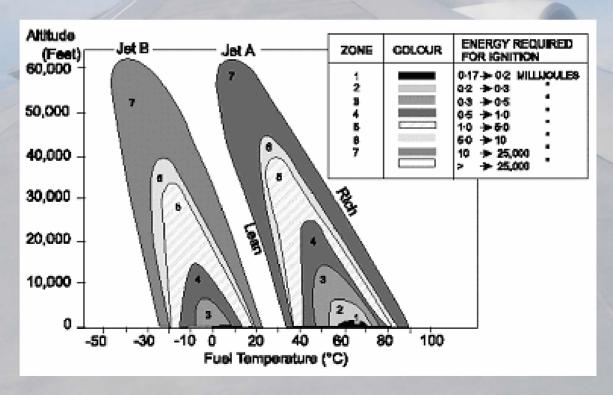
O₂ it is inert.



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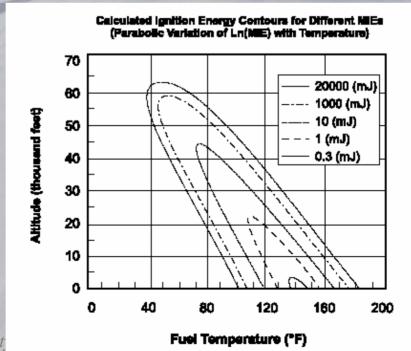
Previous work has shown how flammability limits vary as a function of ignition energy.



- It follows intuitively that flammability limits will shift in a similar manner as inert gas is added to the fuel tank.
- Thus, if your fuel tank is only partially inerted, the flammability exposure time has still been reduced by a significant amount.
- How can this be quantified, validated and built into the flammability model?

Computed Flammability Limits as a Function of O₂

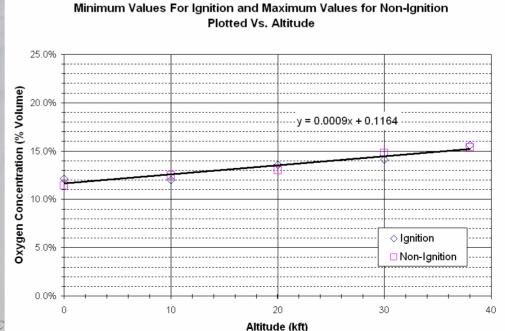
Similar methodology as that in DOT/FAA/AR-98/26 to compute flammability limits as a function of MIE.



Computed Flammability Limits as a Function of O₂

Correlation of the variation of LOC with altitude.

• Previously determined with a large (~20 J) spark source.

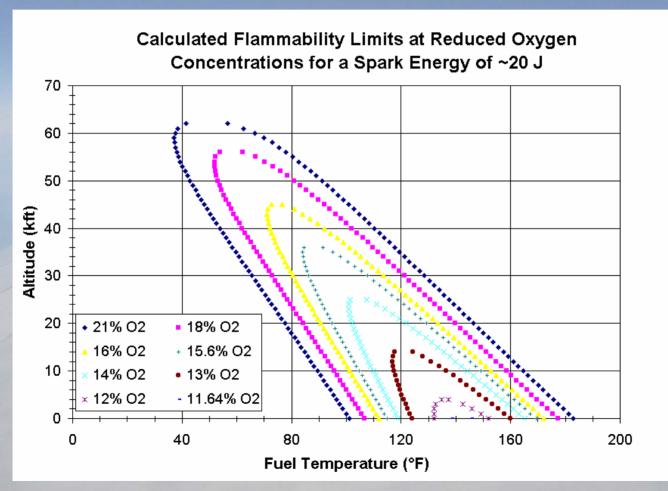


Computed Flammability Limits as a Function of O₂

$$T_{\text{Fuel}} = T_{\text{min}} \pm \sqrt{\frac{\text{Ln}(O_2) - \text{Ln}(O_{2\text{min}})}{a}}, \text{ where}$$

- T_{min} is the minimum of the parabola given by $T_{min} = T_{fp} + 22 1.5Z$.
- a is a constant, determined by matching the curve as best as possible to the calculated 21%
 O₂ curve for the given ignition energy.

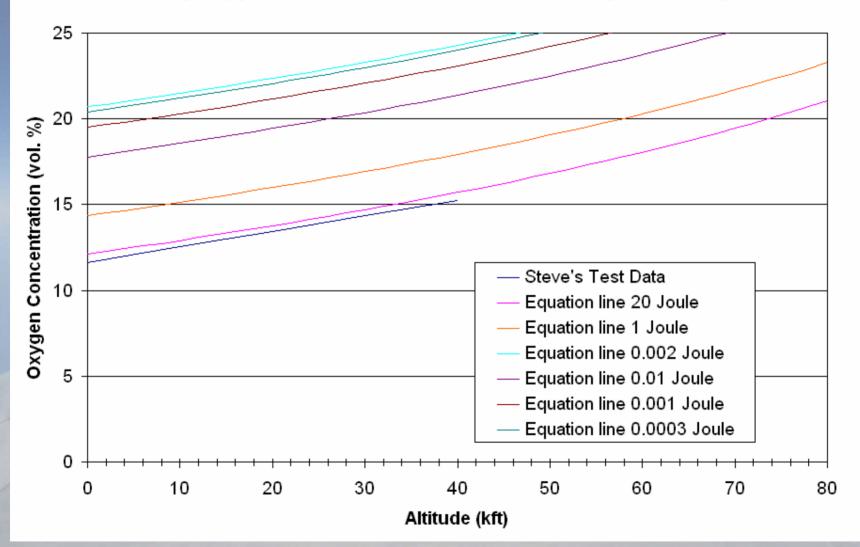
Resultant Curves for a 20 J Calculation



Flammability Limits as a Function of MIE, O₂ and FP

- Combining this with the parabolic MIE calculations and LOC curves for various ignition energies, results in flammability limits which vary as a function of ignition energy, O₂ concentration and flashpoint.
 - The sum of this work was put together into a working MS Excel model by Ivor Thomas

Limiting Oxygen Concentration Curves for Various Ignition Energies





Conclusions

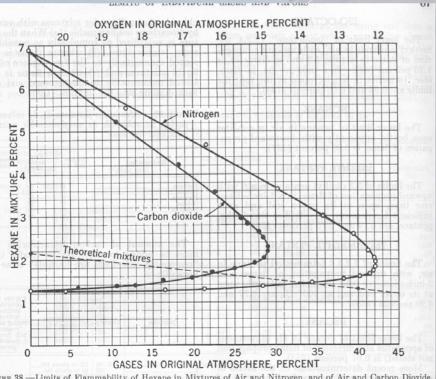
- ➤ By a set of simple calculations, one can obtain varying flammability limits as a function of ignition energy, O₂ concentration and flashpoint.
- Once validated, this data can be used in the flammability model to show reduction in fleet wide fuel tank flammability as a function of the amount of inert gas added to the tank.
- Tests to validate these calculations are planned at the technical center.

Combustion Sphere Testing

- Our current method for ignition testing of Jet-A fuel vapors is extremely time consuming (up to as long as 2 hours per test).
- If a gaseous mixture was available to simulate the flammability properties of Jet A, it would allow us to perform more tests quicker.
- Availability of said mixture would also have applicability to other issues (e.g. explosion proof testing, etc.)

Past Simulants - Hexane

	LFL	UFL	Stoich.	AIT (F)
Hexane	0.033	0.22	0.065	437
JP-8/Jet A	0.032	0.24	0.068	~420



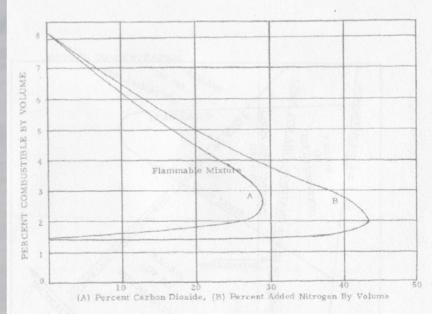


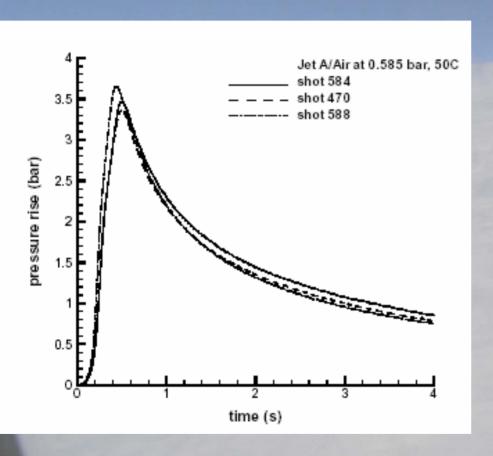
FIG. 2 CONCENTRATION LIMITS OF FLAMMABILITY FOR (A) AVIATION JET FUEL GRADE JP-4 VAPOR-AIR-CO2 MIXTURES, AND (B) AVIATION JET FUEL GRADE JP-4 VAPOR-AIR-N, MIXTURES AT ATMOSPHERIC PRESSURE AND 75°F

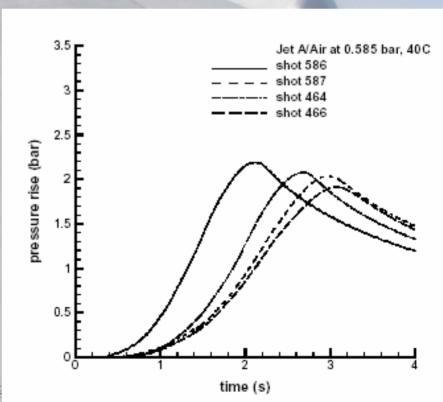
FIGURE 38.—Limits of Flammability of Hexane in Mixtures of Air and Nitrogen, and of Air and Carbon Dioxide.

Past Simulants – Caltech Mixture

- NTSB Docket No. SA-516, Exhibit No. 200
- Volumetric Ratio of H₂:C₃H₈ of 5:1
- Examined the effect of fuel concentration, vessel size and ignition source on pressure history.

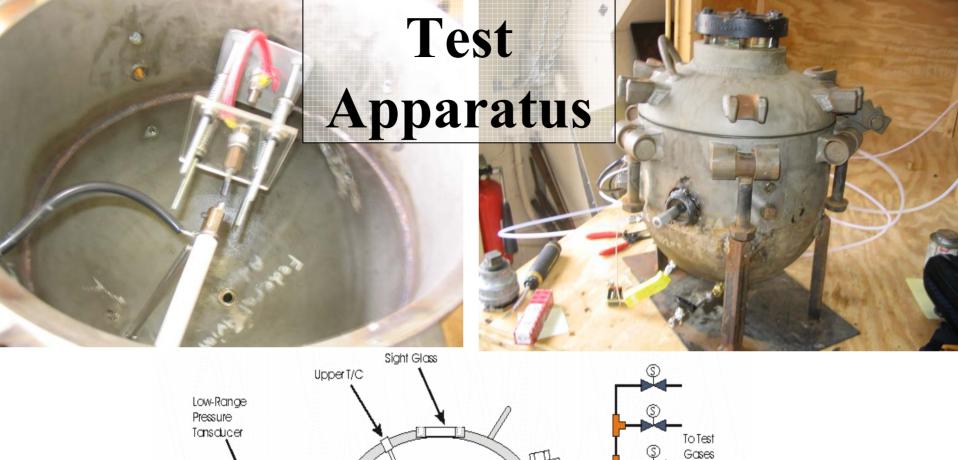
Past Simulants – Caltech Mixture

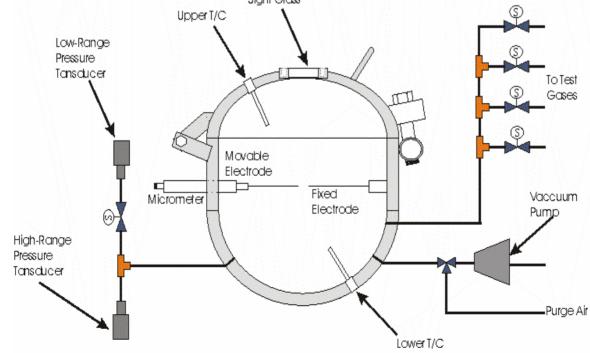




Test Apparatus

- ➤ 20 L combustion vessel constructed with an adjustable spark gap and the ability to utilize various spark/arc sources.
- Tests conducted in a manner similar to the procedures given in ASTM flammability standards (e.g. E582, E2079, etc).

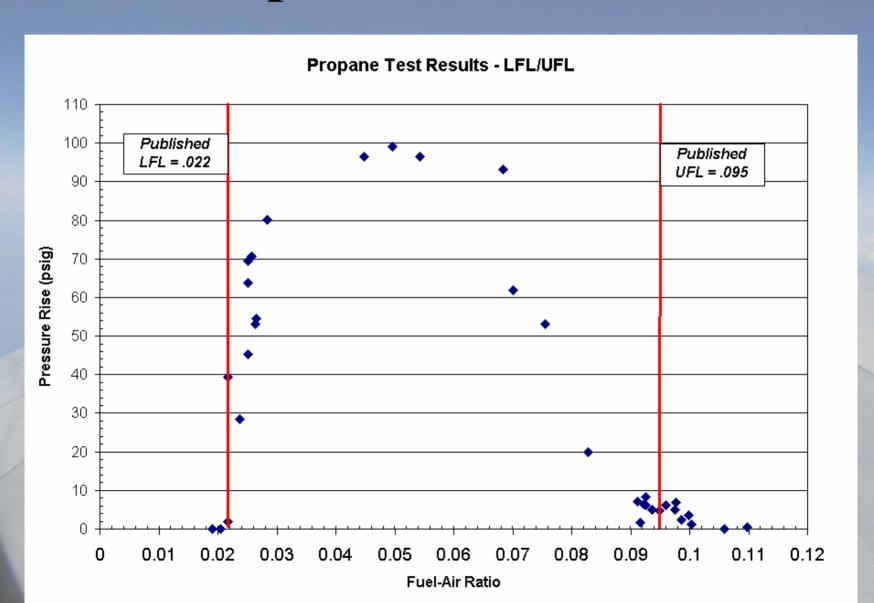




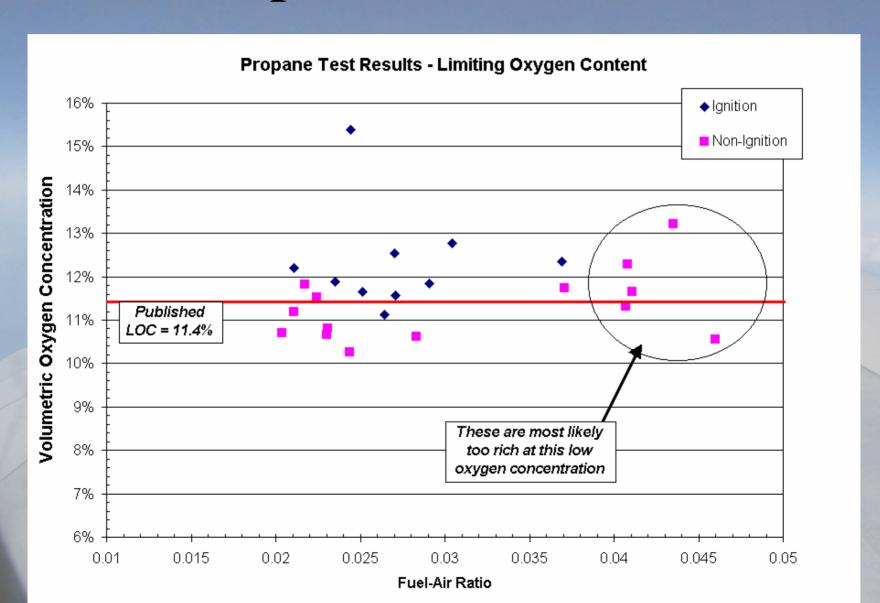
Test Plan

- > Propane testing completed
 - Validation of LFL, UFL and LOC to ensure test article provides accurate results
- Testing with Hexane to be initiated shortly
 - Determination of LOC at reduced pressures

Propane Test Results



Propane Test Results



Future Testing

- Next phase of testing to be conducted with hexane both at sea level and reduced pressures
- Will compare results to the Jet A test results previously acquired to determine its validity as a simulant at reduced pressures
- Once a suitable simulant is determined (hexane or otherwise), the goal is to generate full flammability curve data at various pressures, O₂ concentrations and ignition energies